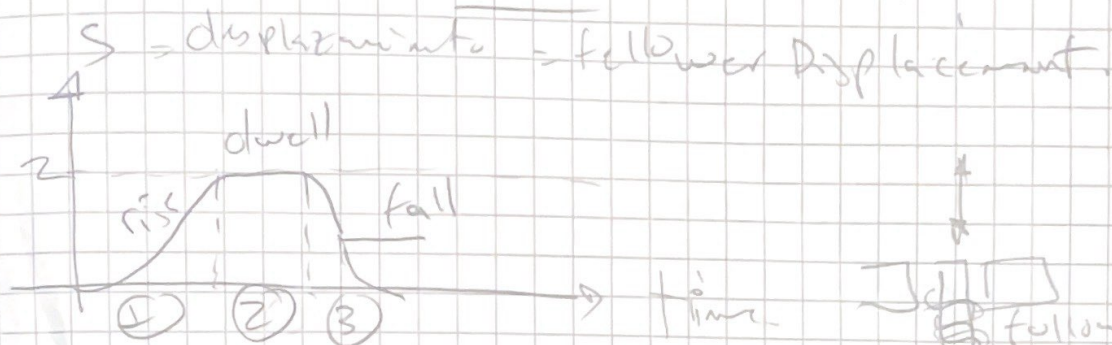


Kinematics of Mechanical System,

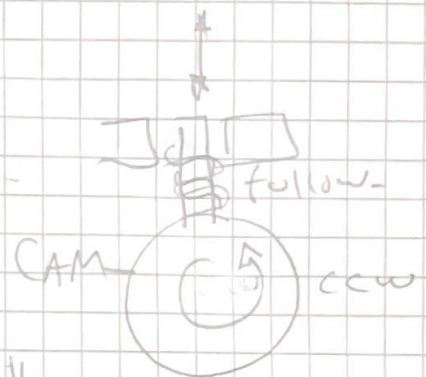
- ① Synthesis of mechanisms
- ② Analysis of mechanisms

| - Position
 | - velocity
 | - acceleration

Comparison: drawing tools. Dimensions



linkage

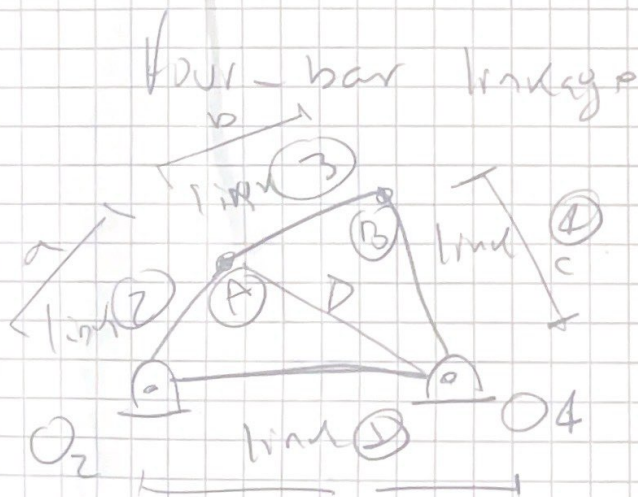


Follow over cam

Cam 4 - Shaft = rotation
link 4

Joints = O_2, O_4, A, B

Links = ①, ②, ③, ④



$$L_4^2 = L_3^2 + d^2 - 2L_3d \cos \theta$$

$$\cos \theta = \frac{L_4^2 - (L_3^2 + d^2)}{2L_3d}$$

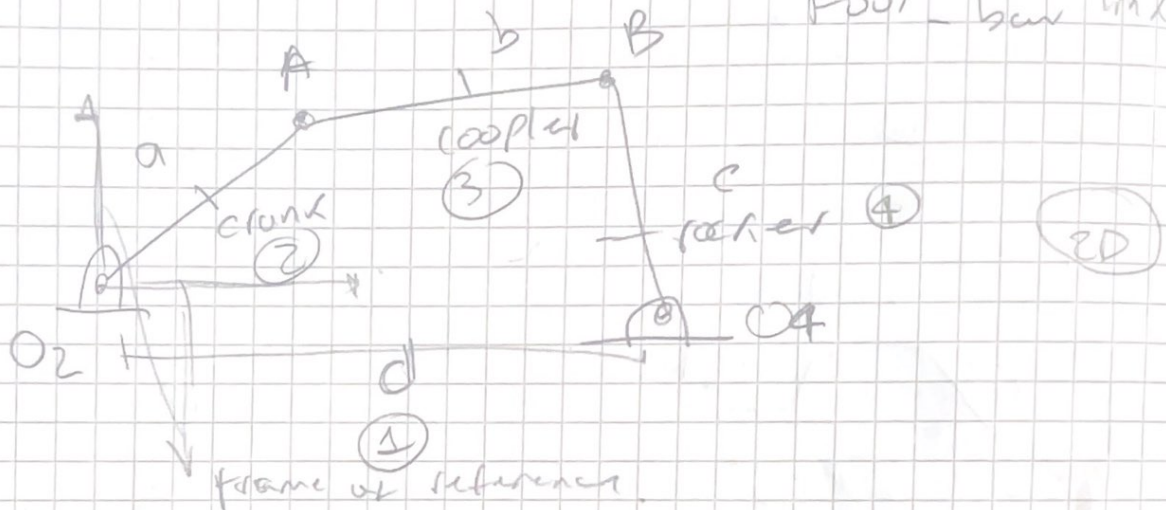
| by Cos | Estimation
 | by Sen. |

$$\sin^2 \theta + \cos^2 \theta = 1$$

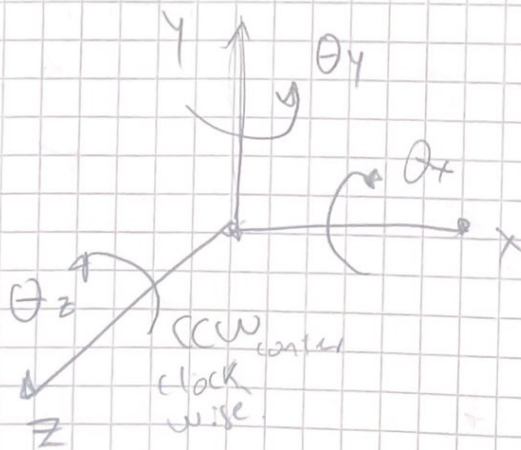
$$\sin^2 \theta = 1 - \cos^2 \theta$$

$$\sin \theta = \sqrt{1 - \cos^2 \theta}$$

Four-bar linkage



todos los puntos fijos representan el enlace 1



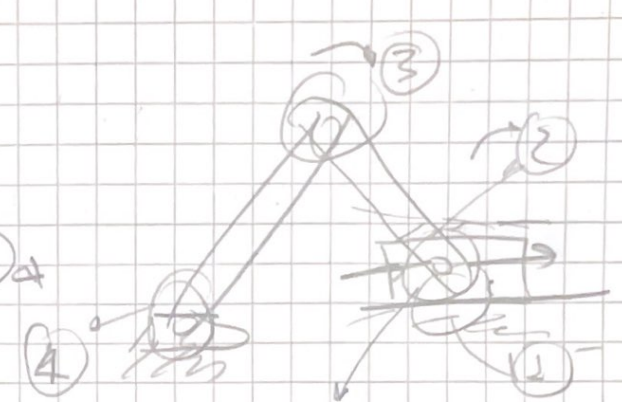
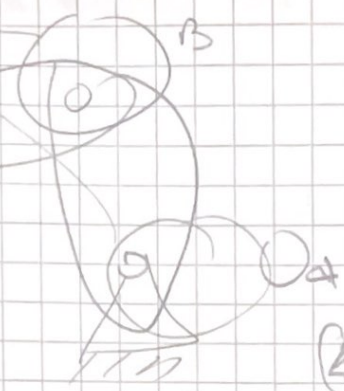
- Join
- links
- Angles

low parts

kinematic pair



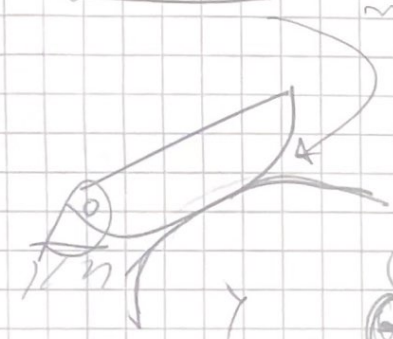
fixed support



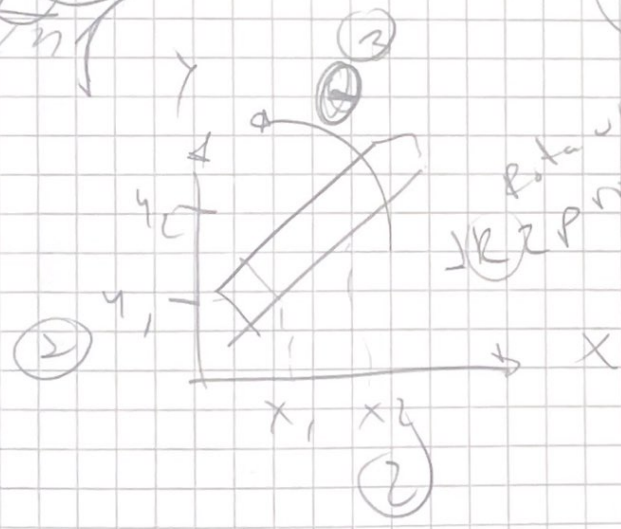
low parts

kinematic pair

High pair: given transmission



high pair



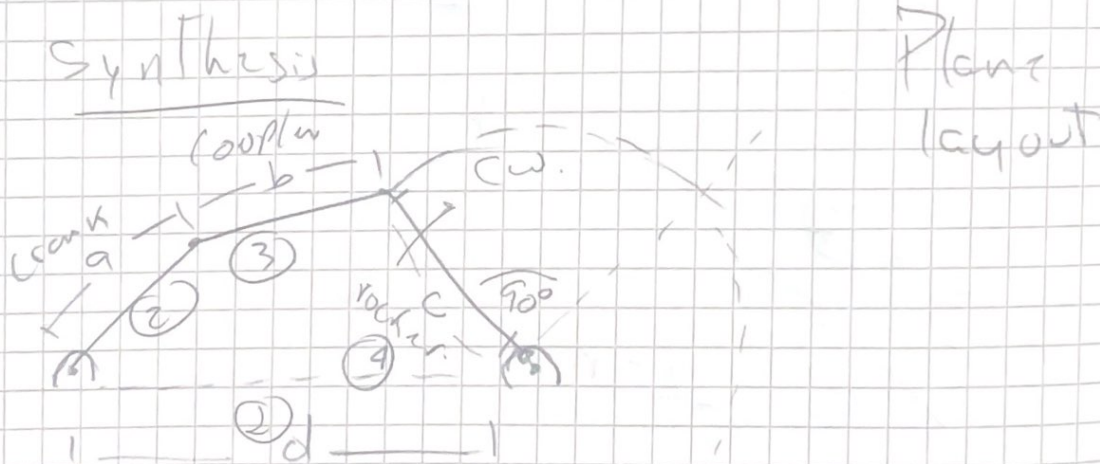
Particular
1R 2P 1C 1C

• Grashof condition ✓

• always results complete or no complete the cond
et crank

Some longitudes to the link are shorter
the longer link $\leq P + Q$

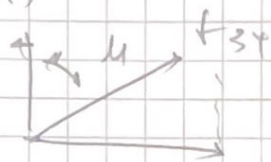
$$S + L \leq P + Q$$



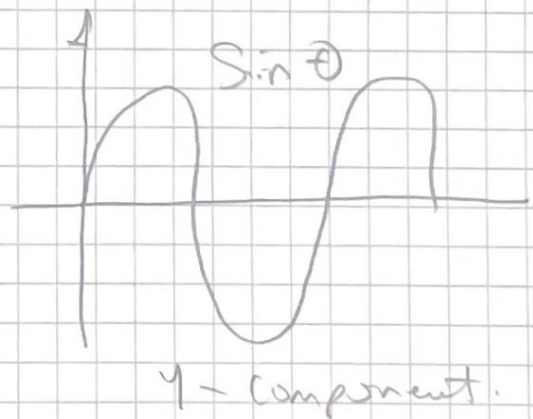
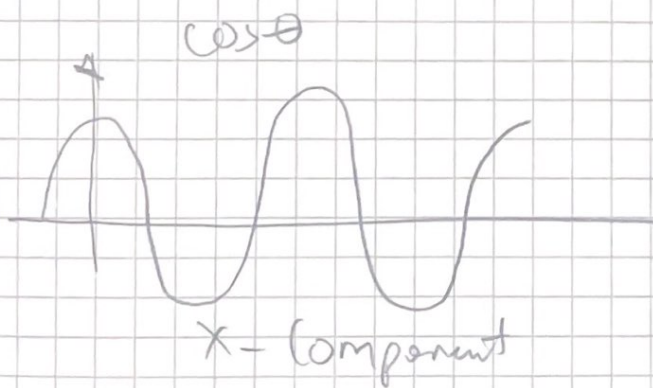
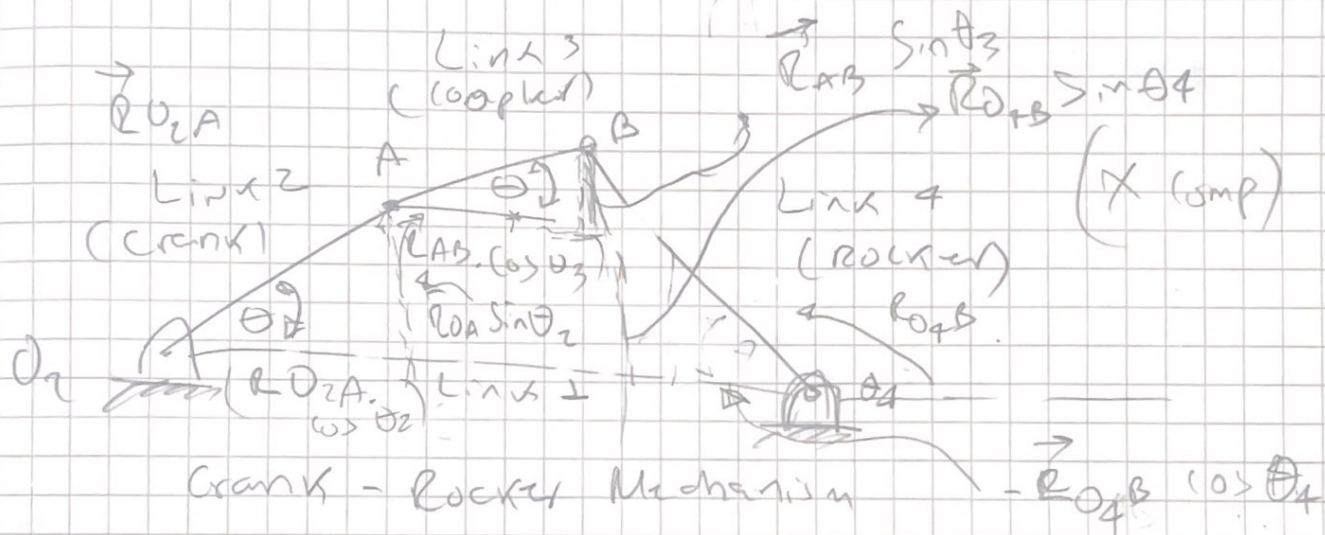
Synthesis Known: $c, 90^\circ$ cw.
rocker link length.

linkwork: a, b, and d

$$f_{horizontal} = f_{34} \cos(\alpha)$$

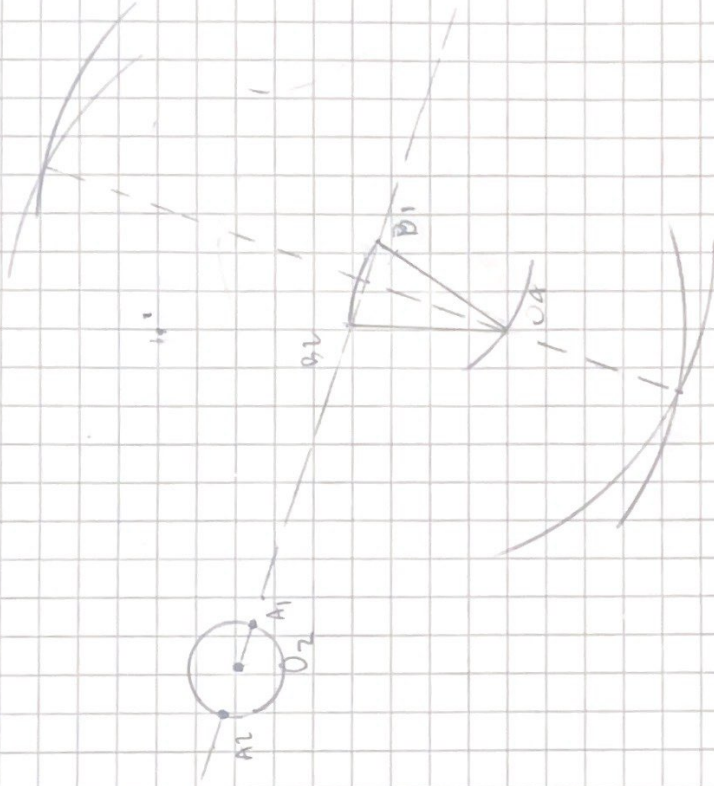


$$f_{34} = \sqrt{f_x^2 + f_y^2}$$



X Comp $\rightarrow$ f function $\rightarrow f(x)$

Y Comp $\rightarrow$ g function $\rightarrow g(x, y)$



Grashof Condition:

$$S + L < P + Q$$

$$62 \text{ mm} < 73 \text{ mm}$$

(2)

(3)

(5)

(1)

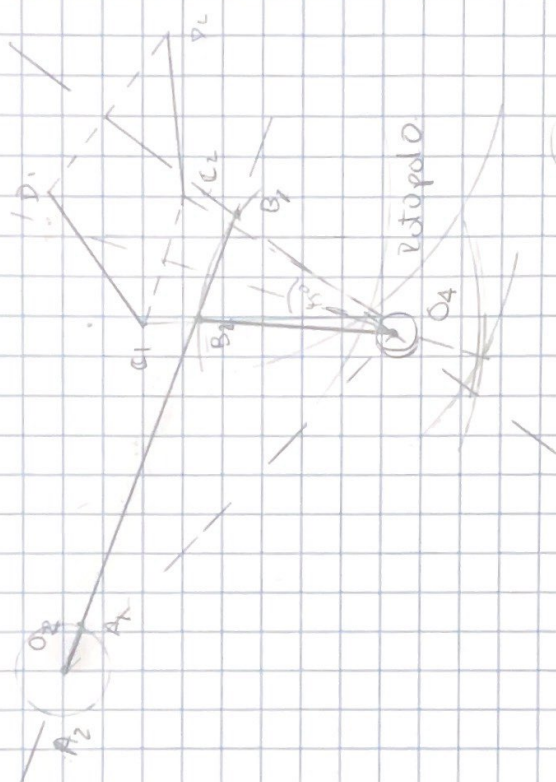
$$\text{Base} (O_2 B_1) = 20 \text{ mm}$$

$$\text{Cam} (A_1 B_1) = 53 \text{ mm}$$

$$\text{Cam} (O_2 A_1) = 6 \text{ mm}$$

$$\text{Link} (O_2 A_1) = 56 \text{ mm}$$

CICR = 130 mm

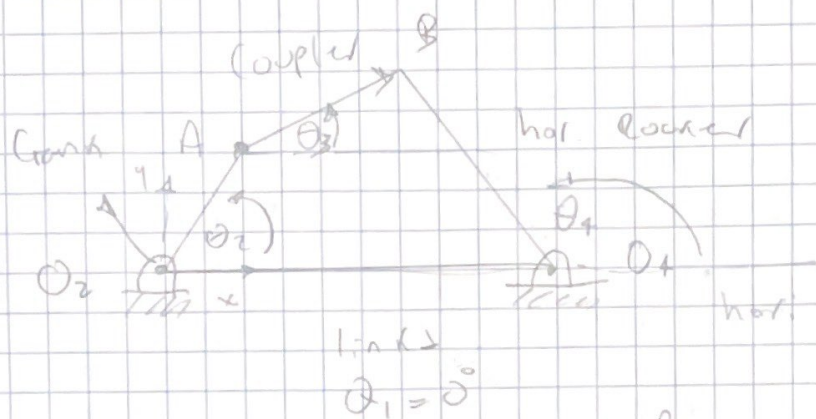


$$130 \leq 130 = 130$$

$$(76 + 59) < (59 + 71)$$

- P Crank: 59 mm
- Q Coupler: 71 mm
- S Slider: 6 mm
- L L1 = 76 mm

Antonio Perez



Displacement of a point

• Position vector

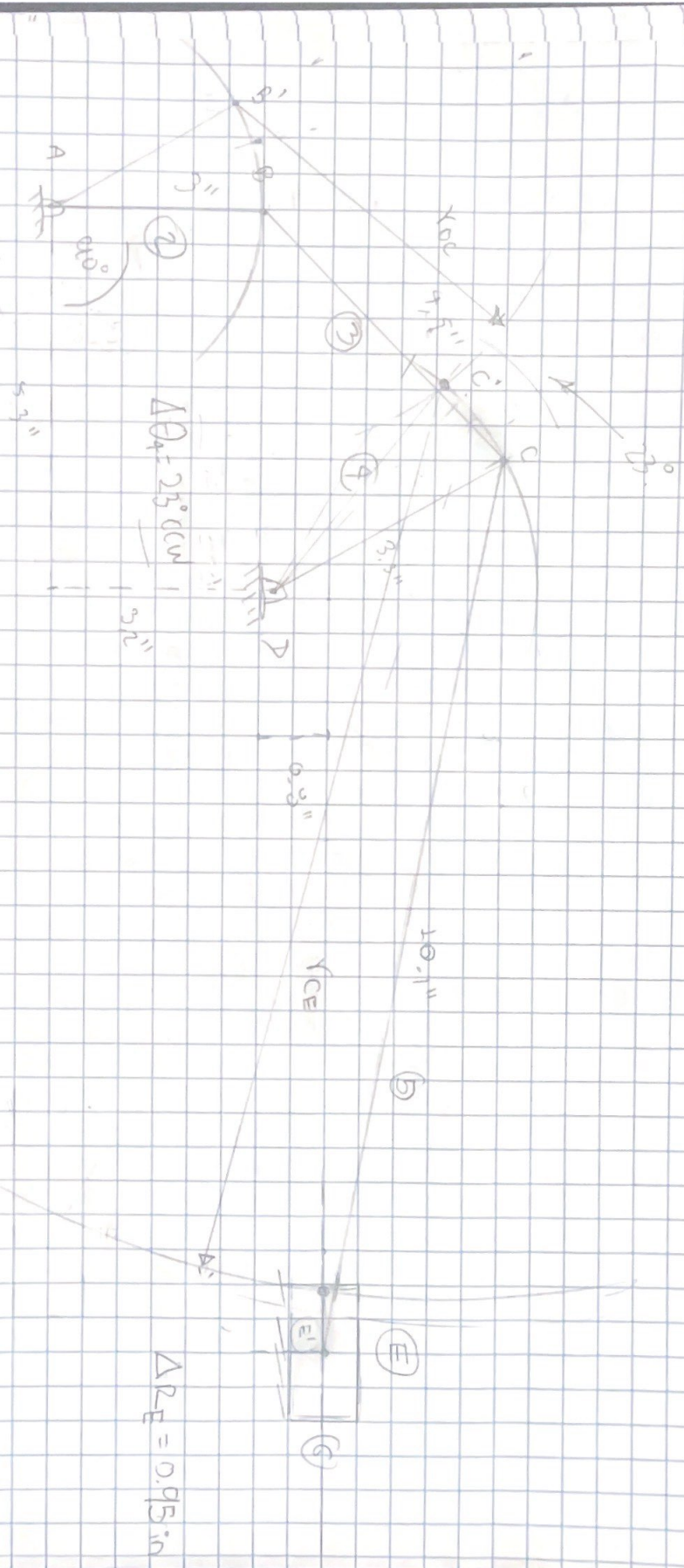
$$\vec{r}_{B/A} = \vec{r}_B - \vec{r}_A +$$

• Closure loop.

r = position

v = velocity

a = acceleration



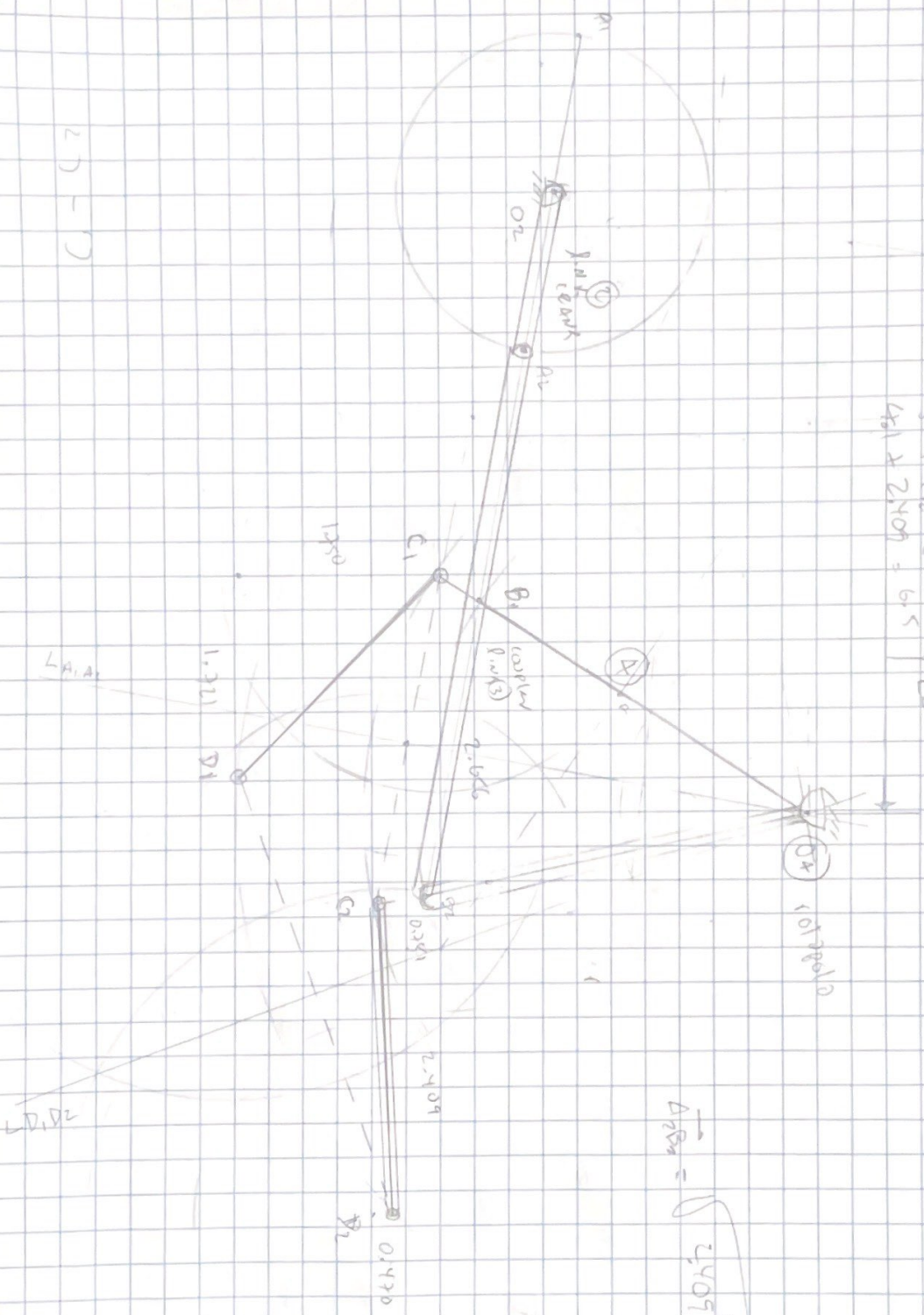
Link (crank) 9.1 in
 Link (bar) 1.2 in
 Link (bar) 2.409 in
 Link 1 5 in
 5 + 1.2 = 6.2 | ext
 4.01 x 2.409 = 9.65 | ext

multi pc
 part (2)

Step 1
 Step 2
 Step 3, etc

$$\Delta R_2 = \sqrt{2.409^2 + 0.411^2}$$

(2) - (1)



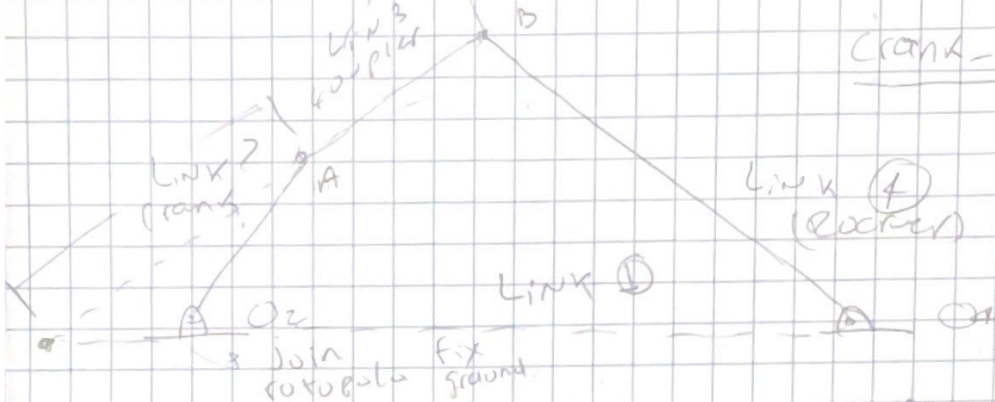
Newton's Law / Power & Velocity

Circular
atom

• method graphical & analytical

• Centro instantaneo de Rotacion (grafico)

CRANK-ROCKER MECHANISM



rotapala
pala ser
isuman
join

$n=4, (\text{LINKS})$

$$C = I C = \frac{n(n-1)}{2}$$

$$= \frac{4(4-1)}{2} = \frac{4 \times 3}{2} = 6$$

rotation

translation

longitudinal

pressure

velocity

acceleration

Ejercicio. Módulo & Velocidad analizado

$$r_{crank}(A) = 3.0 \text{ m}$$

$$\omega_2 = 10.5 \text{ rad/s}$$

$$r_{cpler}(b) = 8.0 \text{ m}$$

$$\theta_2 = 60^\circ \text{ crank}$$

$$r_{cpler}(c) = 6.0 \text{ m}$$

$$\text{Distance entre Grounds (d)} = 7.0 \text{ m}$$

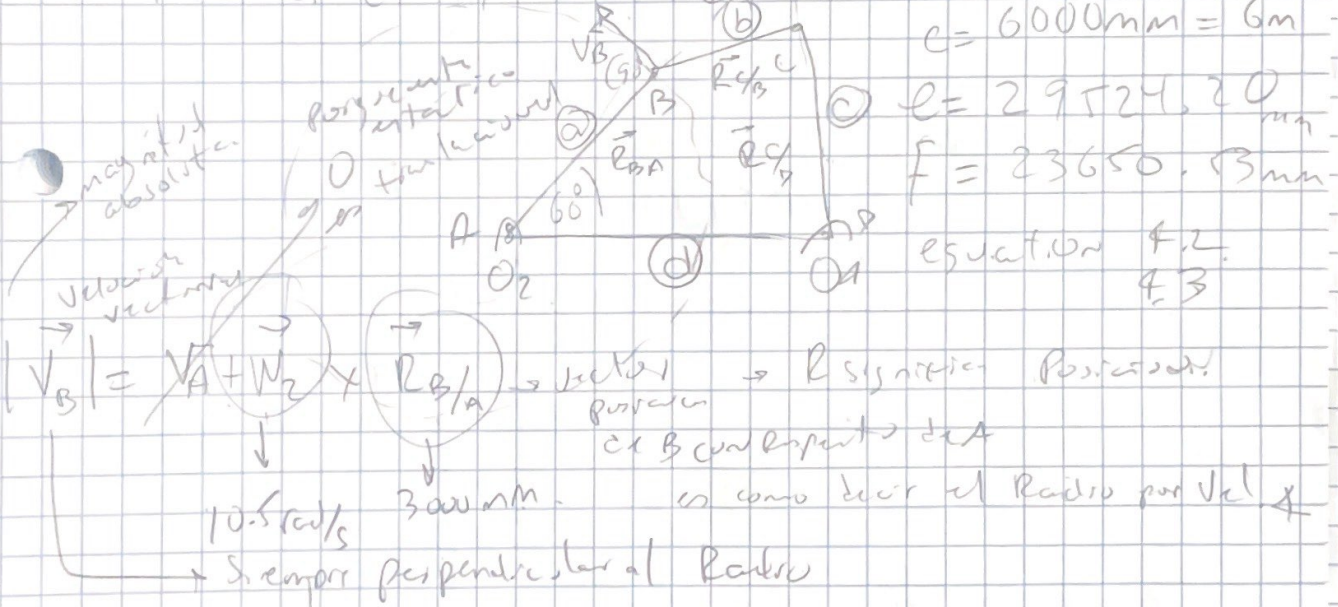
crank Parameters

• magnitude

• Right

• sketch (2 dimensions)

• Centerline (line)



$$|\vec{V}_B| = 10.5 \text{ rad/s} \cdot 3000 \text{ mm} \cdot \frac{1 \text{ m}}{1000 \text{ mm}} = 30.15 \text{ m/s}$$

$$|\vec{V}_B| = 30.15 \text{ m/s}$$

$$|\vec{V}_B| = e \omega_3 \therefore \omega_3 = \frac{|\vec{V}_B|}{e} = \frac{30.15 \text{ m/s}}{29524.70 \text{ mm} \cdot \frac{1 \text{ m}}{1000 \text{ mm}}}$$

$$\omega_3 = \frac{30.15 \text{ m/s}}{29.5244 \text{ m}} = 1.02113 \frac{\text{rad}}{\text{s}}$$

$$\omega_4 = \frac{F}{e} \cdot \omega_3 = \frac{23.650 \text{ mm}}{60 \text{ mm}} \cdot 1.02113 \frac{\text{rad}}{\text{s}} = 4.027 \frac{\text{rad}}{\text{s}}$$

position Analysis
 • Velocity analysis
 $\theta_2 = 60^\circ$
 $a = 3 \text{ m/s}$
 $b = 8 \text{ m/s}$
 $c = 6 \text{ m/s}$
 $d = 2 \text{ m/s}$
 $\theta_3 = ?$
 $\theta_4 = ?$

• Metodo Newton Ranson

• Guess Values; Para iniciar las iteraciones
 ↳ iteración 1

• Para correr el software en matlab (./file script)
 para activarlo doble click

• Para que se invente el computador

• Nueva función

position angles: 22.8120
 71.7975



Input (enter) θ_2 graph
 Velocity (m/s)
 analysis (m/s)

Numerical
 differential equation

el metodo de
 calculo a partir
 de la iteracion
 inicial

θ_3	θ_4
10	60

No es la
 Solucion
 correcta

22.81° | 71.79°

el metodo converge a

Acceleration Polygon:

- 1.1 ① Analysis of position:
- 1.2 ② Analysis of Velocity:
- 1.3 ③ Analysis of Acceleration:

Secundario
depend del dominio
• Se requiere la
longitud de los
links
• RAZ vector de
posición de A respecto
O2.

① Longitud de los links (Synthesis or design)

- Links - Types
- Joints - Types
- Grashof Condition (eater or no rate)
(transmission angle)
- Grados de libertad → através de una formula
o movilidad modify Kutzbach

Dofs or Mobility $M = 3L - 2J - 3E$

1.1 ② Metodos

$$M = 3(L-1) - 2J - 3E$$

- 1.2 ① Metodo Grafico (Graphical approach)
- ② Analitico. → Newton Raphson (NR)
→ Mathematical Model.

harta aca
Polaridad ①

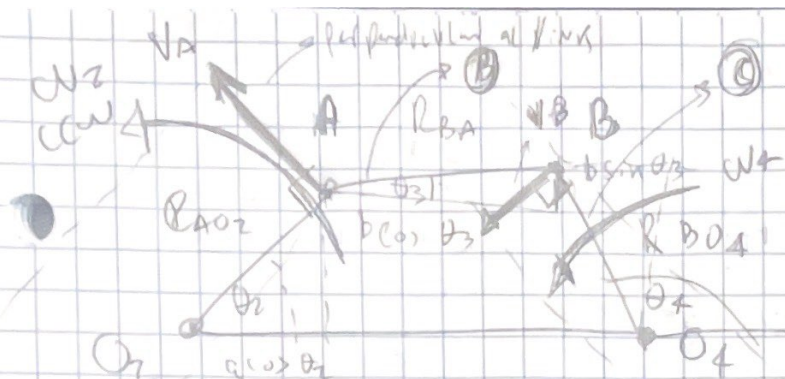
1.3 Acceleration

- ① $\vec{P}$ Posición
- ② $\vec{V}$ Velocidad
- ③ $\vec{A}$ Aceleración

RAOZ A end joint
or Origin joint

- El rotapulo
• Solo
del RUCKER

Motion
Generation



$$\begin{aligned} 1. \vec{r} &= \theta_3 \theta_4 \text{ (units)} \\ 2. \vec{V}_A &= \vec{V}_{O2} + \omega_2 \times \vec{r}_{AO2} \\ \vec{V}_A &= \omega_2 \times \vec{r}_{AO2} \\ 3. \vec{V}_B &= \vec{V}_A + \omega_3 \times \vec{r}_{BO4} \\ \vec{V}_B &= \omega_4 \times \vec{r}_{BO4} \\ \vec{V}_B &= \omega_4 \times \vec{r}_{CO4} \end{aligned}$$

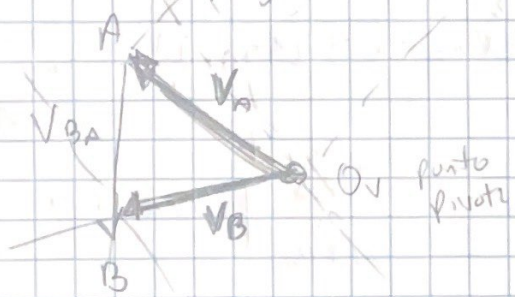
- $\theta_3 =$ es desconocido. } Posición Angular
- $\theta_4 =$ es desconocido. } Posición Angular

Nota: Las longitudes son conocidas gracias a la posición posición y el ángulo de sentido de rotación

$r_{AO2} + r_{BA} - r_{BO4} - r_{CO4} = 0$ (loop closure equation)

La derivando esta fórmula tenemos la velocidad

Para obtener el polígono de aceleraciones



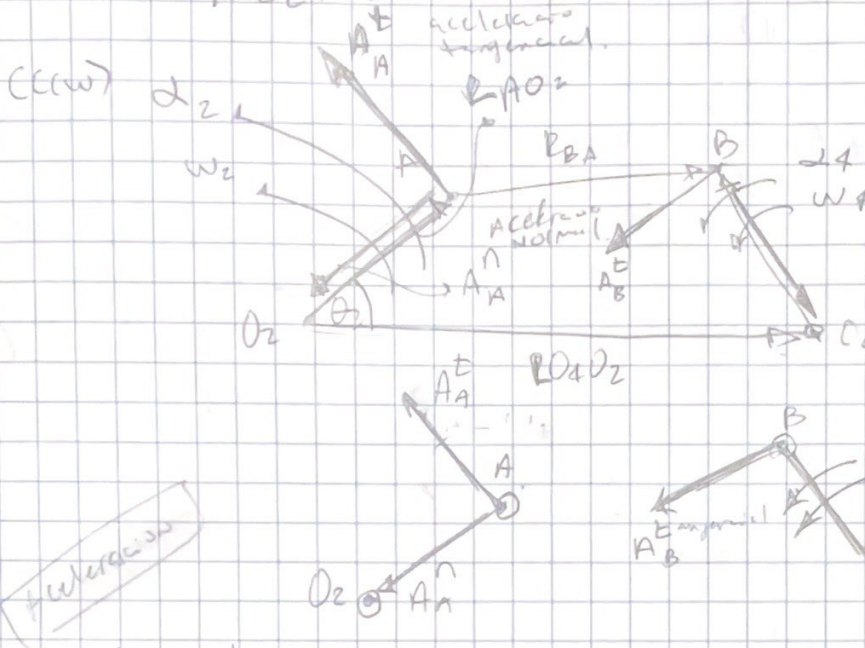
• Siempre del (CRANK (punto pivote) O_2)
Depende si es CW o CCW
arbitrario en cuanto los símbolos.

Velocidad

$$\vec{V}_A + \vec{V}_{BA} - \vec{V}_B = 0$$

Velocity Polygon

Acc en plus avec la acceleration.



• Acceleration tangential, mlt direction de α_2

• Acceleration Normal, is sempre contraire al vector $\vec{R}_{AO_2}$

Acceleration

$$\vec{A}_A^n + \vec{A}_A^t + \vec{A}_{BA}^n + \vec{A}_{BA}^t - \vec{A}_B^n - \vec{A}_B^t = 0$$

$$-w_2^2 \vec{R}_{AO_2} + \alpha_2 \vec{L}_{AO_2} - w_3^2 \vec{R}_{BA} + \alpha_3 \vec{L}_{BA} - (-w_4^2 \vec{R}_{BO_4}) - \alpha_4 \vec{L}_{BO_4} = 0$$

$$\underbrace{-w_2^2 \vec{R}_{AO_2} + \alpha_2 \vec{L}_{AO_2} - w_3^2 \vec{R}_{BA} - (-w_4^2 \vec{R}_{BO_4})}_{\text{know}} + \underbrace{\alpha_3 \vec{L}_{BA} - \alpha_4 \vec{L}_{BO_4}}_{\text{UNKNOWN}} = 0$$

$$\left. \begin{array}{l} w_2, w_3, w_4, \alpha_2 \\ \vec{A}_A^n, \vec{A}_A^t, \vec{A}_{BA}^n, \vec{A}_B^n \end{array} \right\} \text{ know.}$$

$$\left. \begin{array}{l} \vec{A}_B^t \\ \vec{A}_{BA}^t \\ \vec{A}_B \end{array} \right\} \text{ UNKNOWN.}$$

$$\left. \begin{array}{l} \alpha_3 \\ \alpha_4 \end{array} \right\} \text{ UNKNOWN}$$

